# Research on laser in-sky safety early warning method for high power debris laser ranging system 

Xue Dong, Hongyu Long, Zhipeng Liang, Xingwei Han, Jian Gao, Qingli Song, Guohai Zhao, Haitao Zhang<br>Changchun Observatory of National Astronomical Observatories, Chinese Academy of Sciences, Changchun China University of Chinese Academy of Sciences, Beijing China

Email longhy@cho.ac.cn

## ABSTRACT

A method for judging the in-sky safety of the laser beam pointing for high-power debris laser ranging (DLR) system is proposed. It realized the real-time safety area judgment and early warning of the laser beam intersection with the transiting aircraft. We build the laser beam pointing safety warning system at Changchun Station to validate the method.

Results are showed the intersection time between the transiting aircraft and the laser beam accounts for $0.86 \%$ of the observation time, which does not affect the regular operation of the laser ranging system. the energy density of the aircraft outside the intersection area is between $\mathbf{1 0}^{-14} \sim \mathbf{1 0}^{-25}$ $\mathrm{J} / \mathrm{cm}^{2}$, which is much smaller than the laser safety threshold
corresponding to the ANSI Z136 standard. Result shows the effectiveness of the laser in-sky safety warning method on the high-power debris laser ranging system.

## Laser Safety Distance

According to the Maximum Permissible Exposure (MPE) for in DLR systems of different tracking stations are calculated as human eyes given in ANSI Z136.1 standard with equations (1) shown in Table 2. It can be seen that the laser safety distance of and (2), the laser safety distances ( $\mathbf{R}_{\mathrm{SD}}$ ) corresponding to lasers the station $\mathbf{R}_{\mathrm{SD}}$ is usually more than $\mathbf{1 0 0}$ kilometers and covers

$$
R_{S D}=\frac{1}{\varphi} \sqrt{\frac{-D_{f}^{2}}{\ln \left(1-\frac{Q_{M P E}}{Q_{0}}\right)}-a^{2}} \quad(1) \quad \mathrm{Q}_{\mathrm{MPE}}=\operatorname{MPE} \times \frac{\pi \times \mathrm{D}_{\mathrm{f}}^{2}}{4}
$$

In equations (1) and (2), $\varphi$ is the laser emission divergence angle (rad); $\mathbf{Q}_{0}$ is the laser single pulse energy ( $\mathbf{J}$ ); $\mathbf{a}$ is the diameter of the lase beam ( $\mathbf{c m}$ ); $\mathrm{D}_{\mathrm{f}}$ is the pupil diameter of the human eye, which is 7 mm ; MPE $=\boldsymbol{m i n}($ MPE1,MPE $2, \mathrm{MPE} 3)$. The calculation methods of MPE ${ }_{1}$, $\mathrm{MPE}_{2}$, and $\mathrm{MPE}_{3}$ are shown in Table 1, Equations 3 and 4 .

| Tab. 1 MPE $_{1}$ for Point Source Ocular Exposure to a Laser Beam |  |
| :---: | :---: |
| Exposure duration $/ \mathrm{s}$ | $\mathrm{MPE}_{1} / \mathrm{J} \cdot \mathrm{cm}^{-2}$ |
| $10^{-11}$ to $10^{-9}$ | $2.7 t^{0.75}$ |
| $10^{-9}$ to $18 \times 10^{-6}$ | $5.0 \times 10^{-7}$ |

MPE $_{2}=1.8 \times \mathrm{t}^{0.75} \times 10^{-3} \mathrm{~J} \cdot \mathrm{~cm}^{-2} \quad(3)$
$\mathrm{MPE}_{3}=n^{0.25} \times \mathrm{MPE}_{1}$
Where $n=F \times t, F$ is the laser frequency, $t$ is the maximum exposure time, 0.25 s .

| Tab.2 The safety distance of the laser at the station |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Name | $\mathrm{MPE} / \mathrm{J} \cdot \mathrm{cm}^{-2}$ | $\varphi /$ acrsec | $Q_{0} / \mathrm{mJ}$ | $\mathrm{a} / \mathrm{cm}$ | $\mathrm{R}_{\mathrm{HD}} / \mathrm{m}$ |
| Graz | $5.0 \times 10^{-7}$ | 5 | 60 | 6 | 161231.28 |
| Shanghai | $5.0 \times 10^{-7}$ | 12 | 250 | 1 | 137146.12 |
| Kunming | $5.0 \times 10^{-7}$ | 8 | 300 | 82 | 410895.18 |
| Changchun | $5.0 \times 10^{-7}$ | 5 | 500 | 1.5 | 465489.36 |

## Measures Taken

Through the analysis of the station laser, it can be seen that certain measures are needed to ensure the safety of the transit aircraft during the laser ranging operation. Here, the laser pointing Safe angle calculation method as shown in Equations (5) - (7) is proposed to define the safety zone for transit

$$
\begin{gathered}
\Omega=\left(\omega_{1} \pm \omega_{2}\right) \Delta \mathrm{t}+\arctan \left(\frac{L}{R}\right) \\
L=\omega_{R}+\sqrt{\frac{Q_{0}}{10 \pi M P E}} \\
w_{R}=\frac{a}{2} \sqrt{1+\left(\frac{\lambda R}{\pi\left(\frac{a}{2}\right)^{2}}\right)^{2}}
\end{gathered}
$$

(5)
(6)
(7)

Where $\omega_{1}$ is the apparent angular rate of the aircraft; $\omega_{2}$ is the angular rate of the tracking telescope; $\Delta t$ is the extrapolation time (the warning setting time), with a margin; $\mathbf{R}$ is the slant range between the aircraft and the telescope; $L$ is the laser safety radius corresponding to the laser beam at a distance from R , and defines the energy $\mathbf{Q}_{\mathrm{L}}=$ MPE of the radiation received by the aircraft at L ; $w_{R}$ is the effective cross-sectional radius of the base mold at a distance of $R ; \lambda$ is laser wavelength.
aircraft, as shown in Fig 1 (The laser outlet is the center, $2 \Omega$ is the safety angle, the laser safety distance $R_{\text {SD }}$ is the generatrix, the circumvention zone is comprised by the laser danger range corresponding to the internal laser safety threshold(red zone in the figure) and the external warning range divided by
the angular velocity of the aircraft and telescope(orange zone in the figure)). And a laser beam pointing safety warning system is set up at Changchun station to test the method, as shown in Fig 2.



Fig. 1 The laser is directed at the safety zone


Fig. 2 The laser beam is pointed at the security warning system

## Data Analysis

A one-week-long experiment was conducted (from August 8 to August 14, 2022). In this experiment, real ADS-B trajectories were collected to intersect with real space-debris passes. The total observation time, the number of transiting aircraft, the
number of observed passes, and the laser block time are laser radiation energy received by the transiting aircraft in shown in Table 3. Figure 3 shows the starting point azimuth, the safety zone are analyzed separately. azimuth distribution and distance distribution when aircraft position coincides with laser beam and. Figure 4 shows the

| Tab.3 Observation records |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Date <br> (Y.M.D) | Observation <br> Time <br> (s) | Number of <br> aircraft <br> crossings <br> (n) | Number of <br> observed debris <br> passes(n) | Laser block <br> time <br> (s) | Block time <br> ratio <br> (\%) |
| $2022 / 08 / 08$ | 33098 | 45 | 46 | 105.70 | 0.32 |
| $2022 / 08 / 09$ | 38412 | 151 | 44 | 265.70 | 0.69 |
| $2022 / 810$ | 17089 | 153 | 23 | 260.78 | 1.53 |
| $202 / 288 / 11$ | 5640 | 102 | 12 | 100.68 | 1.79 |
| $2022 / 08 / 12$ | 14001 | 128 | 22 | 257.70 | 1.84 |
| $2022 / 08 / 13$ | 16502 | 153 | 19 | 78.69 | 0.48 |
| $2022 / 08 / 14$ | 14702 | 178 | 21 | 124.12 | 0.84 |
| Total | 139444 | 910 | 187 | 1193.37 | 0.86 |



Fig. 3 All-sky avoidance distribution of laser beams


Fig. 4 The range of energy that aircraft receives

## CONCLUSION

The safety of lasers in different DLR system is analyzed and the laser pointing Safe angle calculation method is proposed. The Changchun station laser beam pointing safety warning system was set up. According to the experiment, intersection
$10^{-14} \sim 10^{-25} \mathrm{~J} / \mathrm{cm}^{2}$, which is much less than the MPE value of Changchun Station's laser. So It provides a theoretical basis and effective avoidance strategy for laser safety early warning of high-power DLR system.

