SECTION III: RETROREFLECTOR ARRAY INFORMATION:

A prerequisite for accurate reduction of laser range observations is a complete set of pre-launch parameters that define the characteristics and location of the LRA on the satellite. The set of parameters should include a general description of the array, including references to any ground-tests that may have been carried out, array manufacturer and whether the array type has been used in previous satellite missions. So the following information is requested:

Retroreflector Primary Contact Information:

Name:
Organization and Position:
Address:
Phone No.:
E-mail Address:
Array type:
Single reflector Spherical Hemispherical/Pyramid Planar
other (specify:)
Attach a diagram or photograph of the satellite that shows the position of the LRA, at the end of this document.
□ Attached
Attach a diagram or photograph of the whole LRA at the end of this document.

Attached Same as above, Not attached (acceptable only for a cannonball satellite)

Array manufacturer:

Link (URL and/or reference) to any ground-tests that were carried out on the array:

Has the LRA design and/or type of cubes been used previously?

No Yes (List the mission(s):

)

For accurate orbital analysis it is essential that full information is available in order that the 3dimensional position of the satellite center of mass may be referred to the location in space at which the laser range measurements are made. To achieve this, the 3-D location of the LRA phase center must be specified in a satellite-body-fixed reference frame with respect to the satellite's mass center. In practice this means that the following parameters must be available at 1 mm accuracy or better.

Define the satellite-body-fixed XYZ coordinates (i.e. origin and axes) on the spacecraft: (specify) (add a diagram in the attachment)

Relate the satellite-body-fixed XYZ coordinates to a Celestial/Terrestrial/Solar Reference Frame including the attitude control policy:

(specify) (add a diagram in the attachment)

The 3-D location of the satellite's mass center in satellite-body-fixed XYZ coordinates is: Always fixed at (0, 0, 0) Always fixed at (______, ____) in mm Time-varying by approximately (______) mm during the mission lifetime. Will a time-variable table of the mass center location be available on the web? No Yes (URL: _______

The 3-D location (or time-variable range) of the phase center of the LRA in the satellite-body-fixed XYZ coordinates:

(_____, ____) in mm

The following information on the corner cubes must also be supplied.

The XYZ coordinates referred to in the following are given in: Satellite-body-fixed system (same as above) LRA-fixed system (specify below) (specify the origin and orientation) (add a diagram in the attachment))

List the position (XYZ) of the center of the front face of each corner cube, and the orientation (two angles or normal vector) and the clocking (horizontal rotation) angle of each corner cube. Note that the angles should be clearly defined.

Attached at the end of this document Listed here (acceptable for small number (10 or fewer) of corner cubes) (specify) (add a diagram in the attachment)

Is the corner cube recessed in its container (i.e. can the container obscure a part of the corner cube)? No Yes (specify below)

(specify) (add a diagram)

The s	size (of each	corner cube:	Diameter	() mi	m	Height () mm
1 110	5120	or each	conner cace.	Diameter	(<u> </u>		TTO BILL (/	,

The material from which the cubes are manufactured (e.g. quartz):

The refractive index of the cube material

=

= _____ for wavelength λ = 0.532 micron

= _____ as a function of wavelength λ (micron):

The group refractive index of the cube material, as a function of wavelength λ (micron):

_	for wavelength $\lambda = 0.522$ migran
—	TO EWAVELED IN $\lambda = 0.002$ micron

 $_$ as a function of wavelength λ (micron):

Dihedral angle offset(s) and manufacturing tolerance (in arcseconds):

Radius of curvature of Not applied	of front surfa Yes (sp	aces of cubes:)	
Flatness of cubes' surfaces:						
Back-face coating:						
Uncoated	Coated	(specify the material:)	

Other comments on LRA:

(specify) (add a reference to a study of the optical response simulation/measurement if available) (add a diagram if applicable)



Fig.1 Compass-MS1 satellite and the LRA



Fig.2 LRA of Compass-MS1

The Position of the Compass-MS1 Laser Retro-Reflector Array Phase Center



Vector C is from the satellite coordinate origin to the satellite's center of mass (CoM). Vector L is from the satellite coordinate origin to the mass center of the LRA containing 90 corner cubes.

- C = (-10.1, -8.4, 1177.8) mm.
- L = (602, -80.1, 2418.8) mm.

The plane of the front faces of the cubes is +16.0 mm in the Z direction from the LRA mass center.

The cubes' phase centers are $-h \times n$ in the Z direction from the plane of the cubes.

For the Compass-MS1 cubes, h = 23.3 mm, n = 1.461@532 nm. So phase centers are - 34.0mm in Z.

So z-component of array phase center is (-34.0+16.0) = -18.0 mm from the LRA mass center.

Let L' as the vector from the satellite coordinate origin to the phase center of the LRA. We have

L'= (602, -80.1, 2418.8-18.0) mm, i.e. L'= (602, -80.1, 2400.8) mm

Finally, the vector CP from the satellite center of mass to the phase center of the LRA is CP = L' - CSo CP = (602, -80.1, 2400.8) - (-10.1, -8.4, 1177.8) = (612.1, -71.7, 1223.0) in the satellite fixed frame.

Refractive Index and Dispersion:

Conditions: 22 °C, 760 mm Hg, N ₂					
Wavelength [Vacuum] [nm]	Refractive Index ² n	Thermal Coefficient Δn/ΔΤ ³ [ppm/C]	Polynomial Dispersion Equation Constants', 22 °C		
1128.950	1.448866	9.6	A ₀	2.104025406E+00	
1014.260 n _t	1.450241	9.6	A ₁	-1.456000330E-04	
852.344 n _s	1.452463	9.7	A ₂	-9.049135390E-03	
706.714 n _r	1.455144	9.9	A ₃	8.801830992E-03	
656.454 n _c	1.456364	9.9	A ₄	8.435237228E-05	
632.990	1.457016	10.0	A ₅	1.681656789E-06	
587.725 n _d	1.458461	10.1	A ₆	-1.675425449E-08	
546.227 n _e	1.460076	10.2	A ₇	8.326602461E-10	
486.269 n _F	1.463123	10.4			
435.957 n _g	1.466691	10.6	Sellmeier Dispersion Equation Constants ² , 22 °C		
404.770 n _h	1.469615	10.8	A ₁	0.68374049400	
365.119 n	1.474539	11.2	A ₂ 0.42032361300		
334.244	1.479764	11.6	A ₃	0.58502748000	
312.657	1.484493	12.0			
253.728	1.505522	13.9	B ₁ 0.00460352869		
228.872	1.521154	15.5	B ₂ 0.01339688560		
214.506	1.533722	17.0	B ₃	64.49327320000	
206.266	1.542665	18.1			
194.227	1.558918	20.3	Δn/ΔT Dispersion Equation Constants ³ , 20-25 °C		
184.950	1.575017	22.7	C _o	C ₀ 9.390590	
			C ₁	0.235290	
			C ₂	-1.318560E-03	
			C ₃ 3.028870E-04		
			Other Optical Properties		
			nF'-nC'	0.006797	
			Stress Coeffici	ent 35.0 nm/cm MPa	
			Abbe Constant	ts:	
			V _e	67.6	
			V _d	67.8	

*1 Polynomial Equation: $n^2 = A_0 + A_1 \lambda^4 + A_2 \lambda^2 + A_3 \lambda^{-2} + A_4 \lambda^4 + A_5 \lambda^{-6} + A_6 \lambda^{-8} + A_7 \lambda^{-10}$ with λ in μ m *2 Sellmeier Equation: $n^2 - 1 = A_1 \lambda^2 / (\lambda^2 - B_4) + A_2 \lambda^2 / (\lambda^2 - B_2) + A_3 \lambda^2 / (\lambda^2 - B_3)$ with λ in μ m *3 $\Delta n / \Delta T$ Equation: $\Delta n / \Delta T$ [ppm/C] = $C_0 + C_1 \lambda^{-2} + C_2 \lambda^{-4} + C_3 \lambda^{-6}$ with λ in μ m The above dispersion equations for SiO₂ were fit to the refractive indices of 20 wavelengths from 1129 nm to 185 nm.